

# **Seabottom Acoustics Parameters from Reverberation Vertical Coherence in Shallow Water**

Ji-Xun Zhou and Xue-Zhen Zhang

Georgia Institute of Technology, Atlanta, GA 30332, USA and  
Institute of Acoustics, Chinese Academy of Science, China

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## ABSTRACT

Acoustic reverberation in shallow water involves a two-way sound propagation and boundary scattering process. It must, therefore, contain rich information on seabottom acoustic parameters. Reverberation from one shot offers a continuous spatial sampling of surrounding sound field. Thus, inversion of seabottom acoustic parameters from shallow-water reverberation is very attractive for saving time and cost. Wide band reverberation data have been collected from the first China-US joint ocean acoustics experiment in the Yellow Sea (Yellow Sea '96) and from the Asian Sea International Acoustic Experiment (ASIAEX01) in the East China Sea. Using the R-mode method and introducing a concept of average angular spectrum for sound propagation, Zhou developed a theoretical model for reverberation spatial coherence and average reverberation intensity in shallow water [Zhou, *Acta Oceanologia Sinica*, **1**, No. 2, 212-218 (1979) and *Acta Acustica*, **5**, No. 2, 86-99 (1980)]. In the current paper, this model is converted back to a more familiar summation of normal-modes. With this model, the sound velocity/attenuation in sediments and bottom scattering strength are derived for low- and mid-frequencies from at-sea experimental data (YS78, YS96 and ASIAEX01), including reverberation vertical coherence and average reverberation intensity.

## I. MOTIVATIONS:

### 1. Engineering application

Optimal array processing requires...

### 2. Physics

Forward: how Ocean environments effect on RVC

Backward: inversion of seabottom Acoust. Parameters

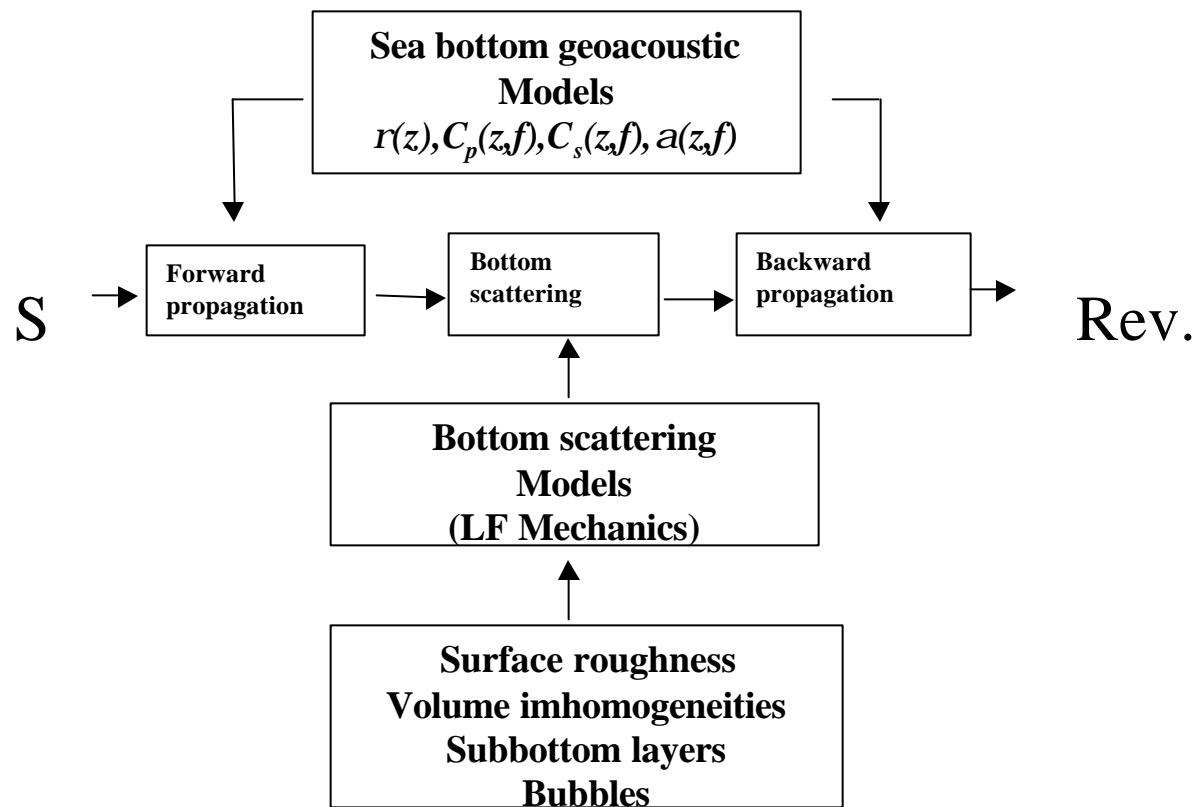
(Rev. derived  $S_b(\theta)$  is often mixed with  
uncertainty of  $C_2$  and  $\alpha_2$ .)

Urick: (1970)  $\rightarrow$  HC/VC measurements

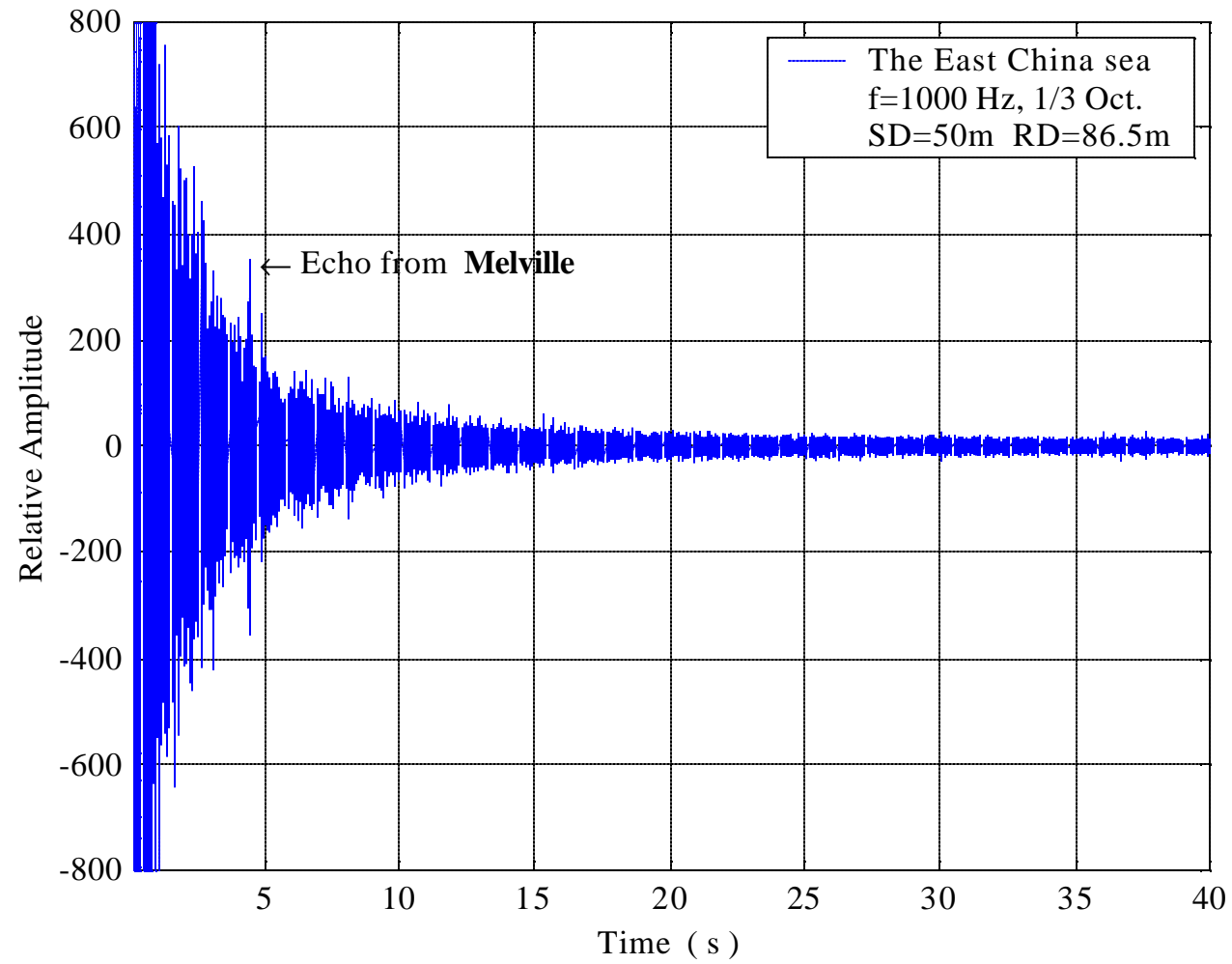
Zhou *et al* (1979,1993,1997)  $\rightarrow$  Model/data

Popov *et al* (1994)]

**Reverberation challenges many basic research topics  
in shallow water**



## Reverberation at SY-3



## II. THORY

The sound field intensity in shallow water can be expressed as a sum of normal modes:

$$\begin{aligned} |\mathbf{y}(r, z; z_0)|^2 = & \frac{2\mathbf{p}}{r} \sum \left\{ \frac{|\Phi_n(z_0)|^2 |\Phi_n(z)|^2}{k_n N_n^2} e^{-2\mathbf{b}_n r} \right. \\ & \left. + \frac{2\mathbf{p}}{r} \sum_{n \neq m} \sum \frac{\Phi_n(z_0) \Phi_m^* \Phi_n(z_0) \Phi_n(z) \Phi_m^*(z)}{k_n^{1/2} k_m^{1/2*} N_n N_m^*} e^{i(k_n - k_m^*)r} \right\} \end{aligned} \quad (1)$$

$$| \Phi_n ( z ) |^2 = \frac{c_1}{k_n \tan \mathbf{q} ( z )}$$

$$k_n = k ( z ) \cos \mathbf{q} ( z )$$

$$2\int_{\mathbf{x}_n}^{\mathbf{h}_n}\sqrt{k^2(z)-k_n^2}dz+\mathbf{e}_{\mathbf{x}_n}+\mathbf{e}_{\mathbf{h}_n}=2n\mathbf{p}$$

$$\frac{d}{dn}\int_{\mathbf{x}_n}^{\mathbf{h}_n}f(z,n)dz=\int_{\mathbf{x}_n}^{\mathbf{h}_n}f_l'(z,n)dz+f(\mathbf{h}_n,n)\frac{d\mathbf{h}_n}{dn}-f(\mathbf{x}_n,n)\frac{d\mathbf{x}_n}{dn}\tag{2}$$



## Angular spectrum expression on average intensity of Shallow-water sound propagation (Brekhovskikh,Zhou)

$$I(r, z; z_0) = \frac{4}{r} e^{-ar} \int \frac{e^{2 \ln |v(\mathbf{q})| r / s(\mathbf{q})}}{S \times \tan \mathbf{q}(z)} d\mathbf{q}(z_0) = \frac{2e^{-ar}}{r} \int I_{aps}(\mathbf{q}, r, z; z_0) d\mathbf{q}(z_0) \quad (3)$$

$$I_{aps}(\mathbf{q}, r, z; z_0) = \frac{2 e^{-2 b_n r}}{S \times \tan \mathbf{q}(z)} = \frac{2 e^{2 \ln |v(\mathbf{q})| r / s(\mathbf{q})}}{S \times \tan \mathbf{q}(z)} \quad (4)$$

weighting process in an angular domain for  
average characteristics in shallow water:  
Sound propagation, Noise, Reverberation  
Spatial coherence, etc.

**Simple  
Intuitive**

## Angular spectrum expression on average reverberation intensity in shallow water

$$\begin{aligned}
 R(r, z; z_0) &= \iint \frac{e^{-ar}}{r} I_{aps}(\mathbf{q}, r, z_h; z_0) \times AM_b(\mathbf{q}, \mathbf{f}) \times \frac{e^{-ar}}{r} I_{aps}(\mathbf{f}, r, z; z_h) d\mathbf{q} d\mathbf{f} \\
 &= \iint \frac{e^{-ar}}{r} \frac{2e^{2\ln|v(\mathbf{q})|r/s(\mathbf{q})}}{S \times \tan \mathbf{q}(z_h)} \times AM_b(\mathbf{q}, \mathbf{f}) \times \frac{2e^{2\ln|v(\mathbf{f})|r/s(\mathbf{f})}}{S \times \tan \mathbf{f}(z)} \frac{e^{-ar}}{r} d\mathbf{q}(z_0) d\mathbf{f}(z_h) \quad (5)
 \end{aligned}$$

$$d\mathbf{q}(z_0) = \frac{2p}{S_n k(z_0) \sin \mathbf{q}_n(z_0)} dn \quad (6)$$

→a summation of normal-modes by

Zhang and Jin (1984,1987)

D.D. Ellis (1994).

## VERTICAL COHERENCE

For sound propagation by Smith (1976) and Zhou(1979):

$$\mathbf{r}_v(\Delta z, r, z; z_0) = \frac{\iint I_{aps}(\mathbf{q}, r, z; z_0) |S(w)|^2 e^{-jk\Delta z \sin(\mathbf{q})} d\mathbf{q} dw}{\iint I_{aps}(\mathbf{q}, r, z; z_0) |S(w)|^2 d\mathbf{q} dw} \quad (7)$$

For reverberation (Zhou,1979):

$$\mathbf{r}_{Rv}(\Delta z, r, z; z_0) = \frac{\int \frac{e^{-2b_n r}}{S \times \tan \mathbf{q}(z)} M[\mathbf{q}(z_h)] [\cos[k(z)\Delta z \sin(\mathbf{q}(z))]] d\mathbf{q}(z_h)}{\int \frac{e^{-2b_n r}}{S \times \tan \mathbf{q}(z)} M[\mathbf{q}(z_h)] d\mathbf{q}(z_h)}$$

$$\begin{aligned}
& \mathbf{r}_{R_v}(\Delta z, r, z; z_0) = \\
& \left\{ \sum_n \frac{e^{-2\mathbf{b}_n r} \cos[k(z)\Delta z \sin \mathbf{q}_n(z)] M[\mathbf{q}_n(z_h)]}{S_n^2 \times \tan \mathbf{q}_n(z) k(z_h) \sin \mathbf{q}_n(z_h)} \right\} \\
& \times \left\{ \sum_n \frac{e^{-2\mathbf{b}_n r} M[\mathbf{q}_n(z_h)]}{S_n^2 \times \tan \mathbf{q}_n(z) k(z_h) \sin \mathbf{q}_n(z_h)} \right\}^{-1} \quad (9)
\end{aligned}$$

$$S_n \approx -2\mathbf{p} / (dk_n / dn) \quad (10)$$

### III. MEASUREMENTS

The experiments were conducted at 3 sites in China Seas by using explosive source with 1 kg gram TNT charges.

Seabed is very flat at YS78/YS96 sites; rather flat at AIAEX01.

The mean grain diameter of sediments:

0.070mm (YS78), 0.0643mm (YS96) and 0.105mm (? ASIAEX01).

Seabed are mainly fine sand-silty sand.

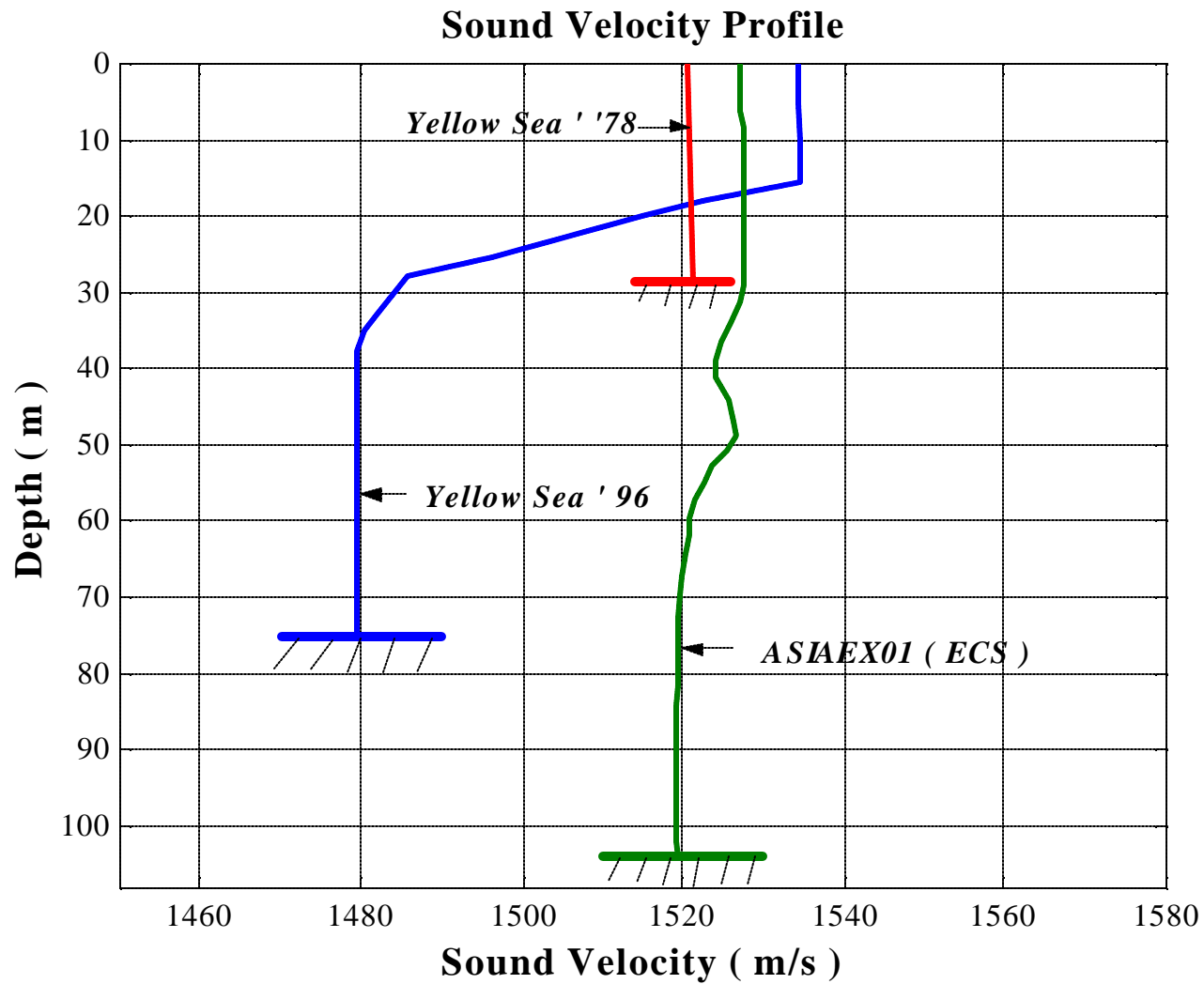
The YS78 data from hydrophones/4-channel analog recorder

The YS96:16 hydrophones/16-channel digital recorder

The ASIAEX01: 32/32

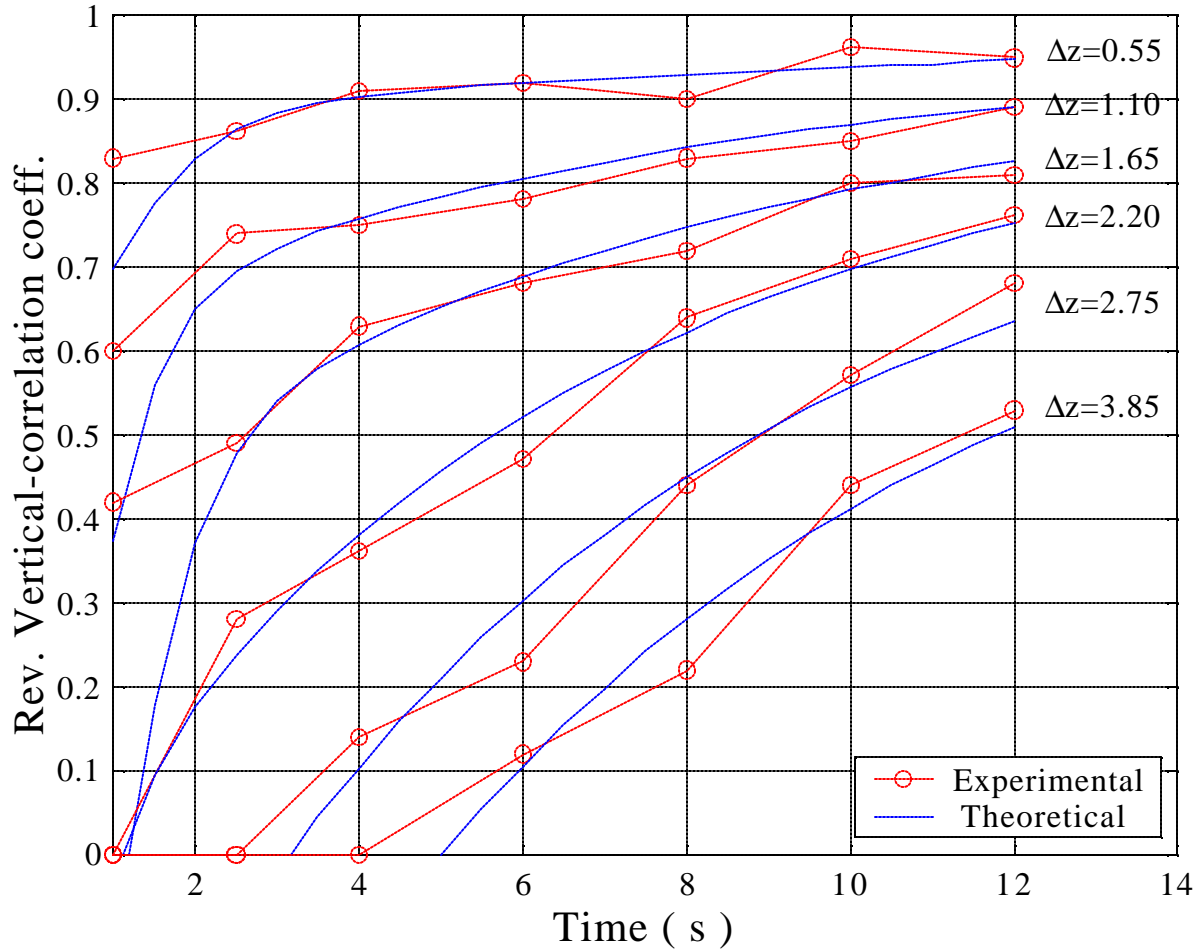
All hydrophone arrays were designed by IOA,  
and suspended from ship

# Sound velocity profiles for YS78, YS 96 and ECS ASIAEX01



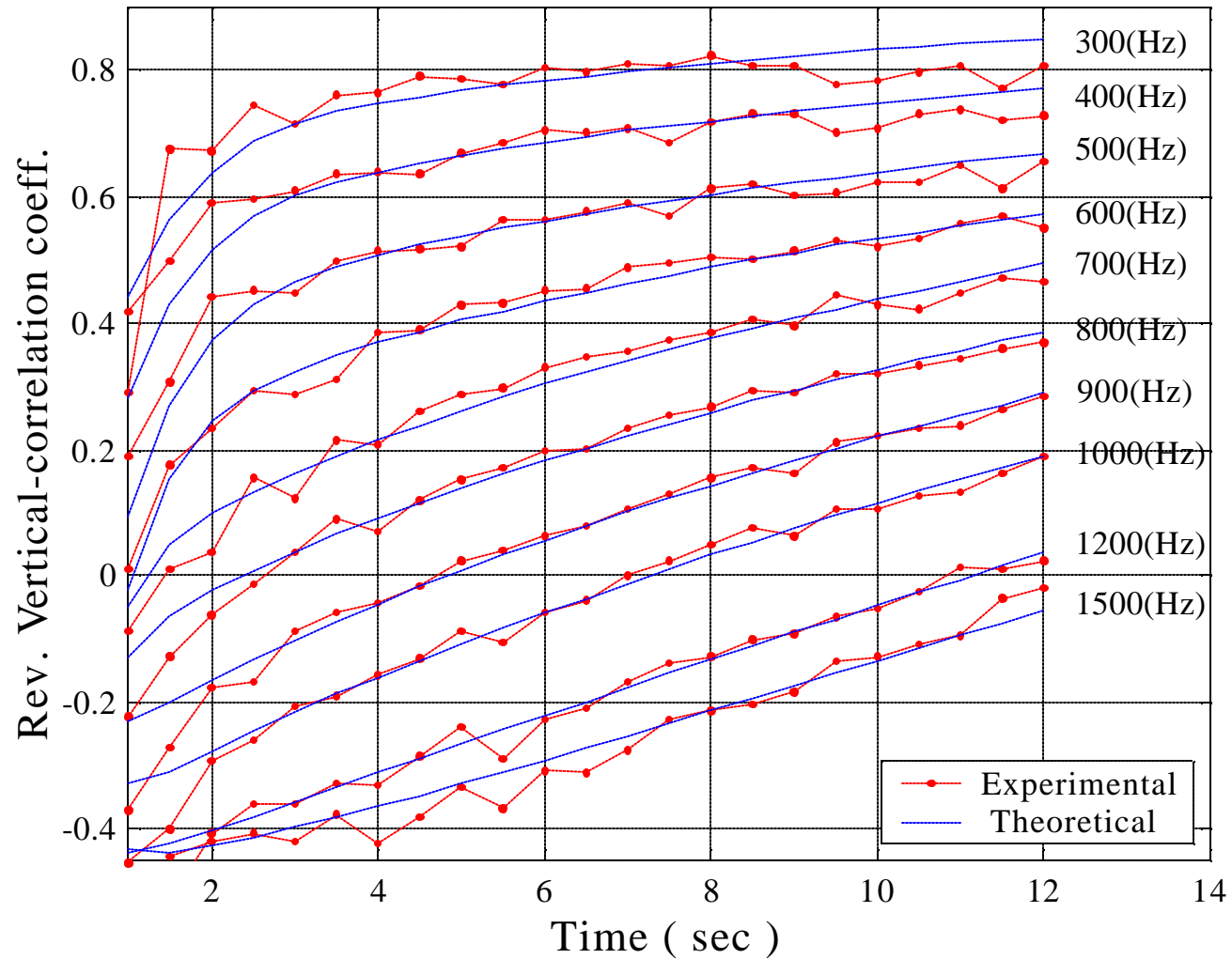
## IV. (a) MODEL/DATA COMPARISONS

Measurement and Prediction,  $F=800$  Hz, Yellow Sea, 10/78



RV coefficients at 800 Hz as a function time and hydrophone separation and  $\Delta z$  in the Yellow Sea, 1978. Data are average values over 12 explosive signals.  $\Delta z=0.55\text{m} - 3.85\text{m}$

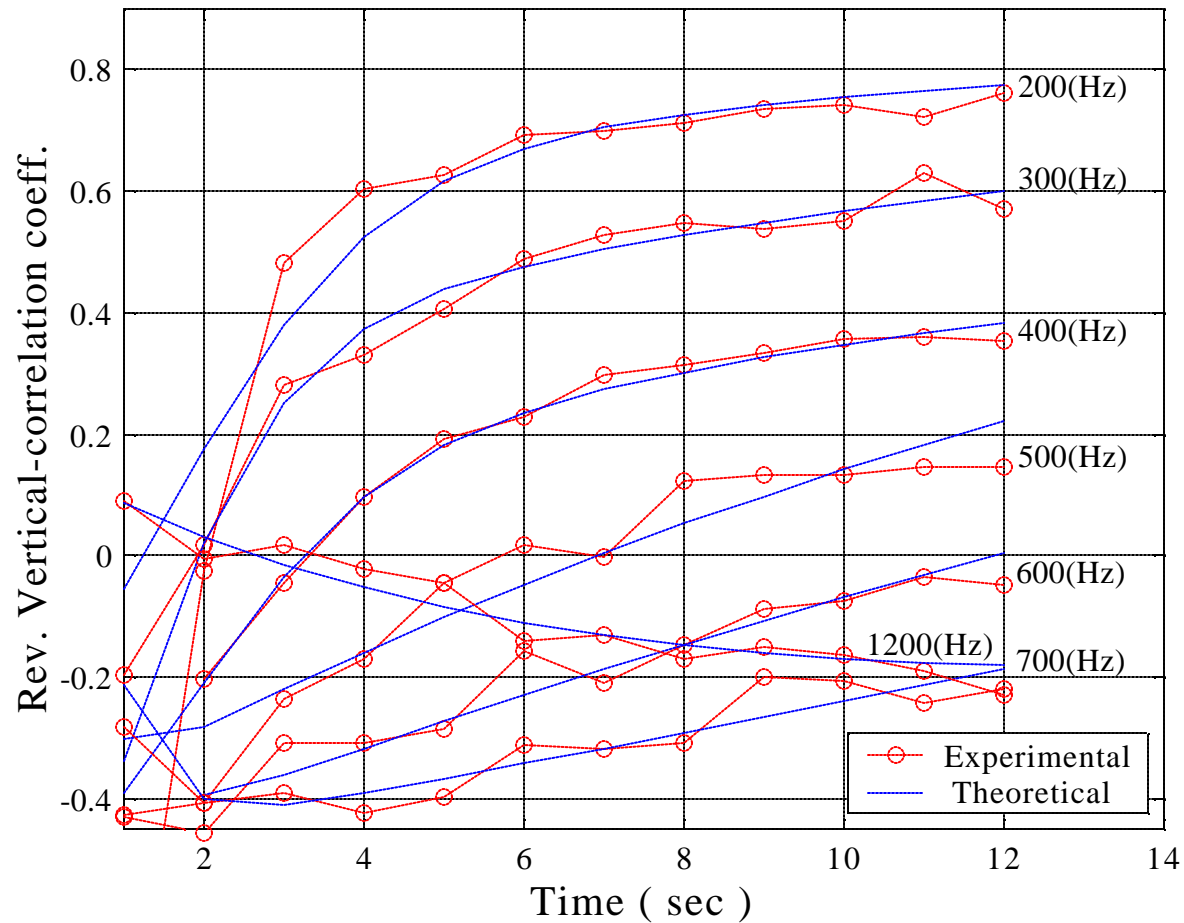
### Measurement and Prediction, Yellow Sea, 08/26/96



RVC as a function of time and frequency in the Yellow Sea, 1996. Hydrophone separation = 2m. The data are average values of 5 shots and 8 pairs of hydrophones, located at depths from 42m to 66m.



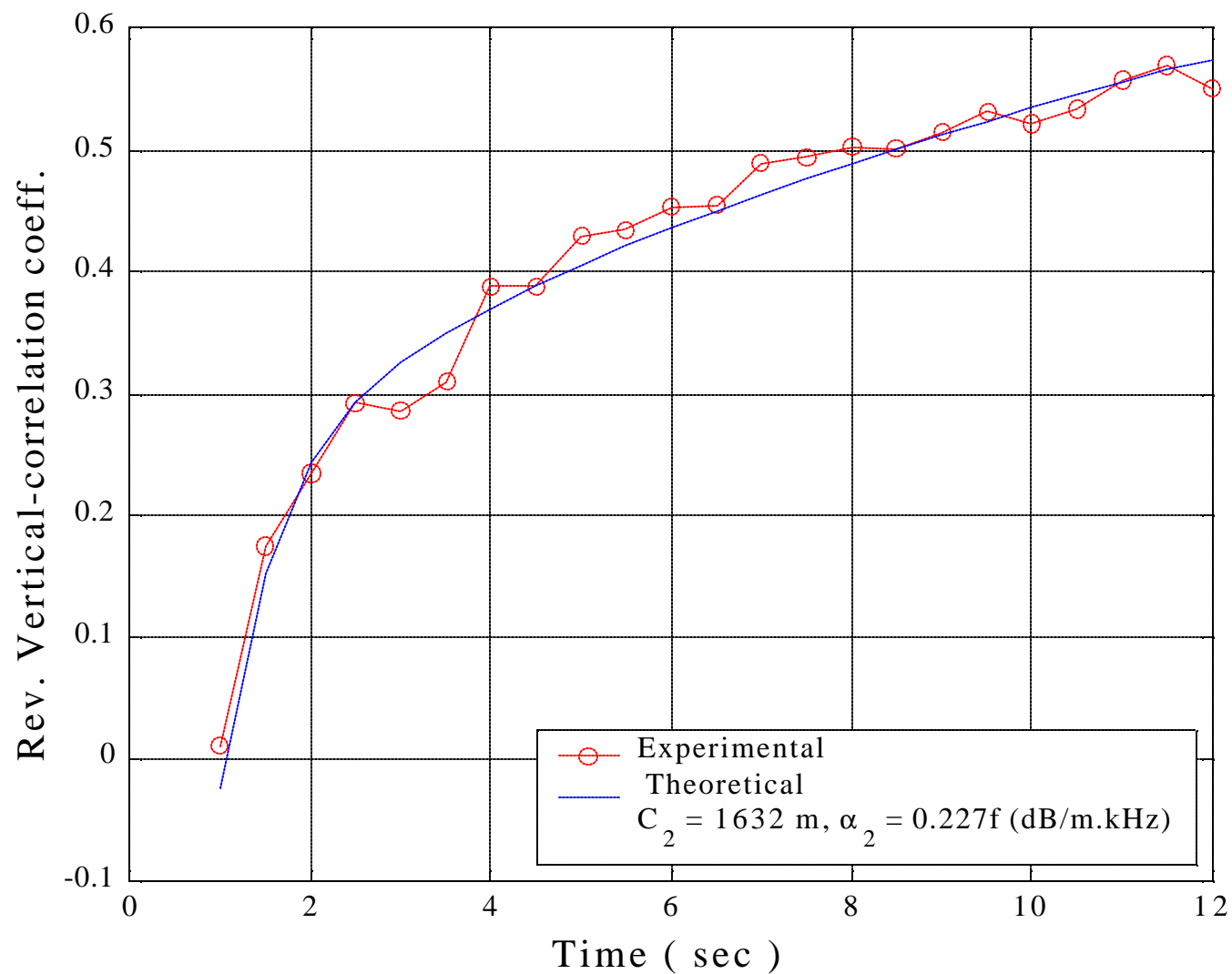
Measurement and Prediction, East China Sea, 06/03/01



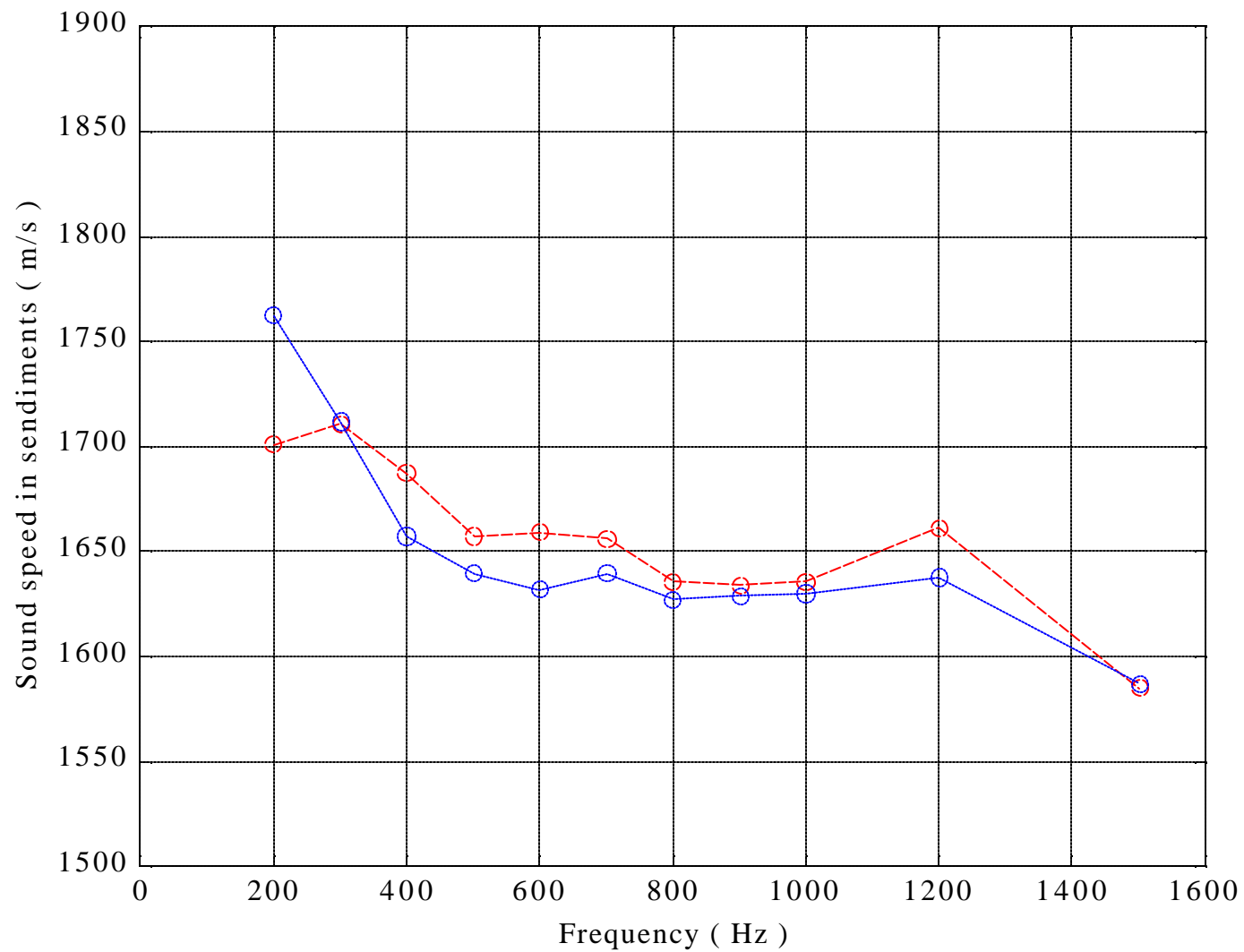
RVC as a function of time and frequency in the East China Sea (ASIAEX01), 2001. Hydroplane separation = 4m. The data are average values of 3 shots and 8 pairs of hydrophones, located at depths from 56.5m to 90.5m.

#### IV. (b) INVERSION OF SOUND SPEED AND ATTENUATION FROM YS96 RVC

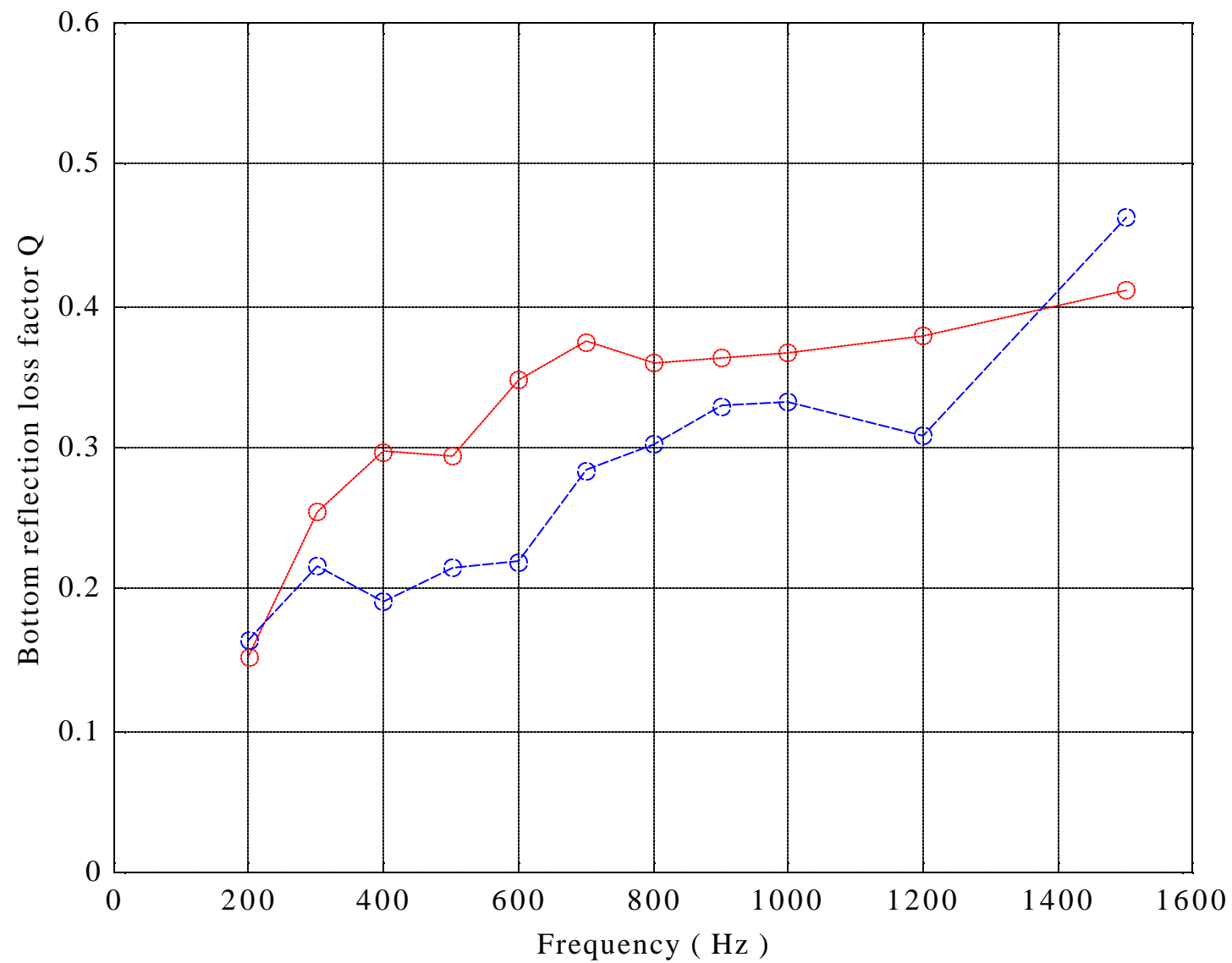
$F = 600 \text{ Hz}$  ,  $dz = 2 \text{ m}$  , Yellow Sea, 08/26/96



Inverted  $C_2$  from Rev.Coherence, Yellow Sea,08/26/96

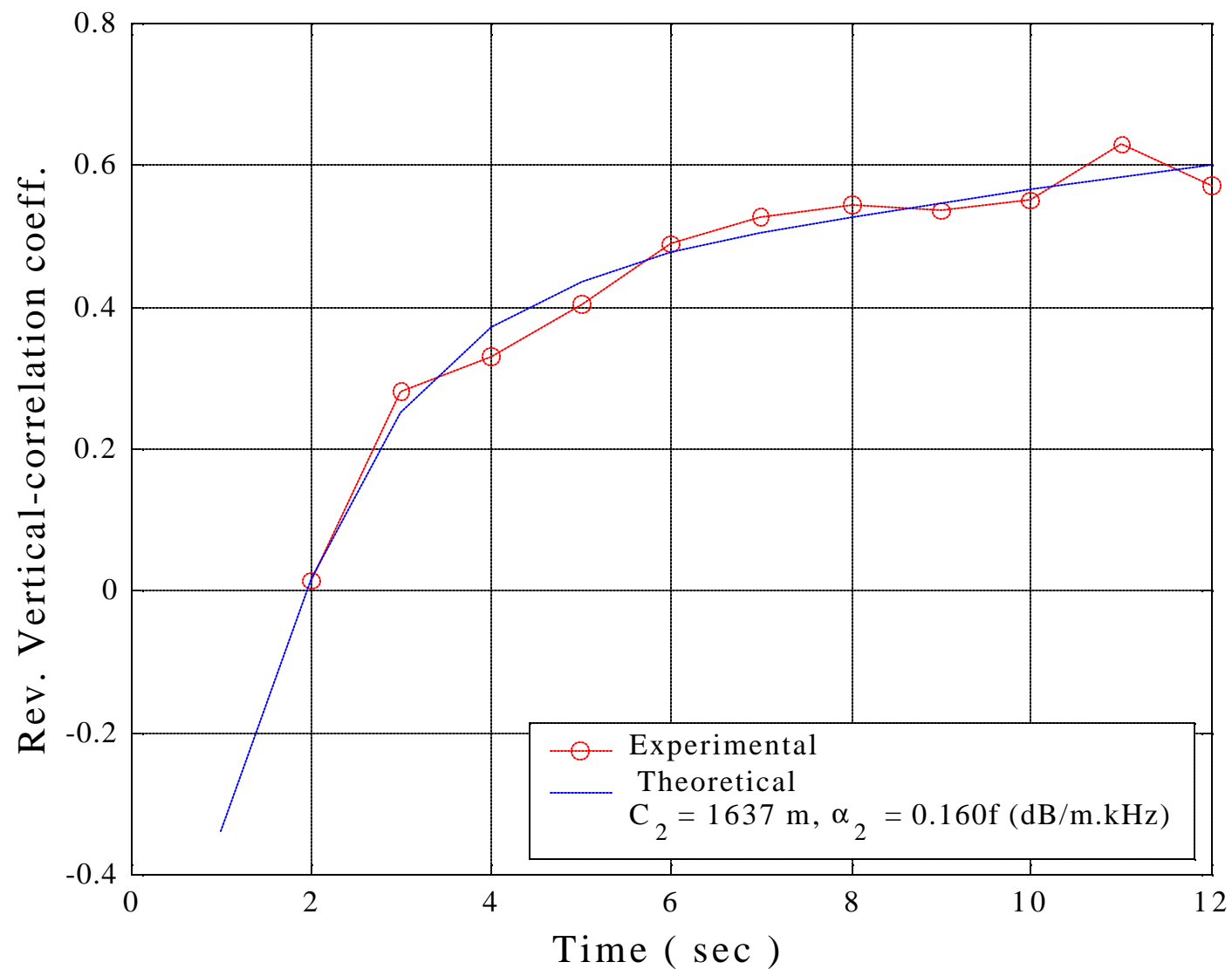


seabed reflection coefficient -  $\ln |V(\theta)| = Q \theta$

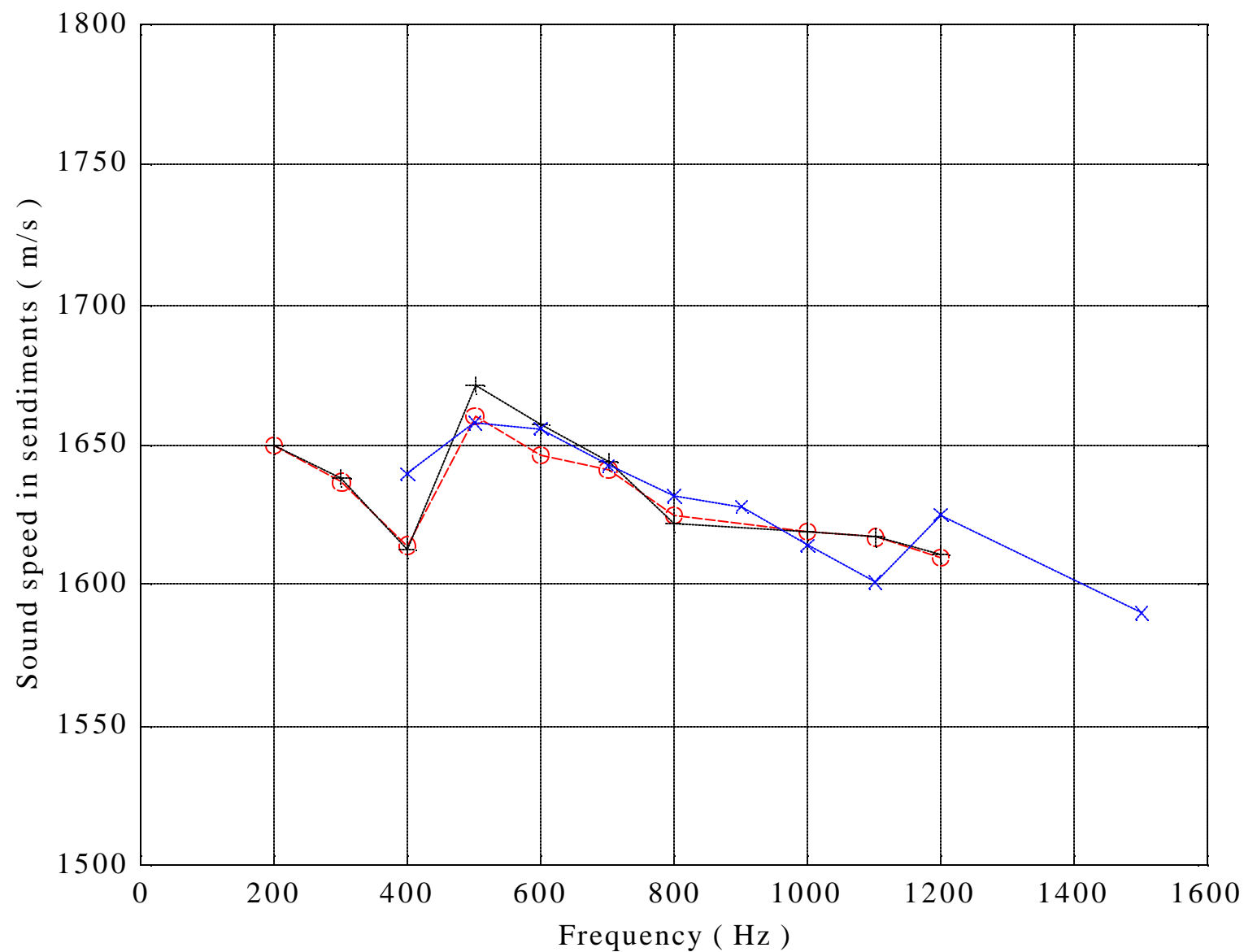


(c) INVERSION OF SOUND SPEED AND ATTENUATION  
FROM ASIAEX01 RVC

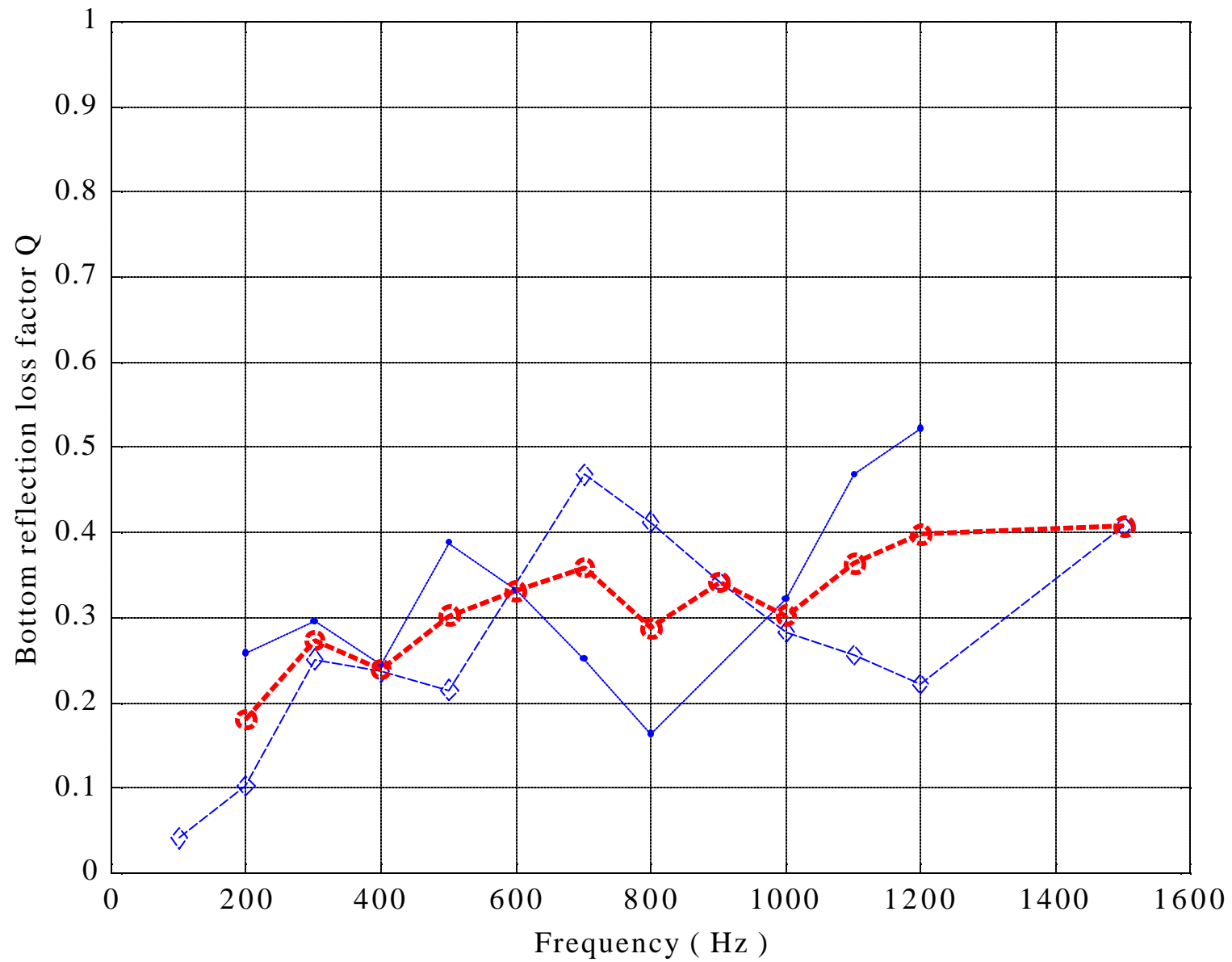
$F = 300 \text{ Hz}$ ,  $dz = 4 \text{ m}$ , East China Sea, 06/03/01

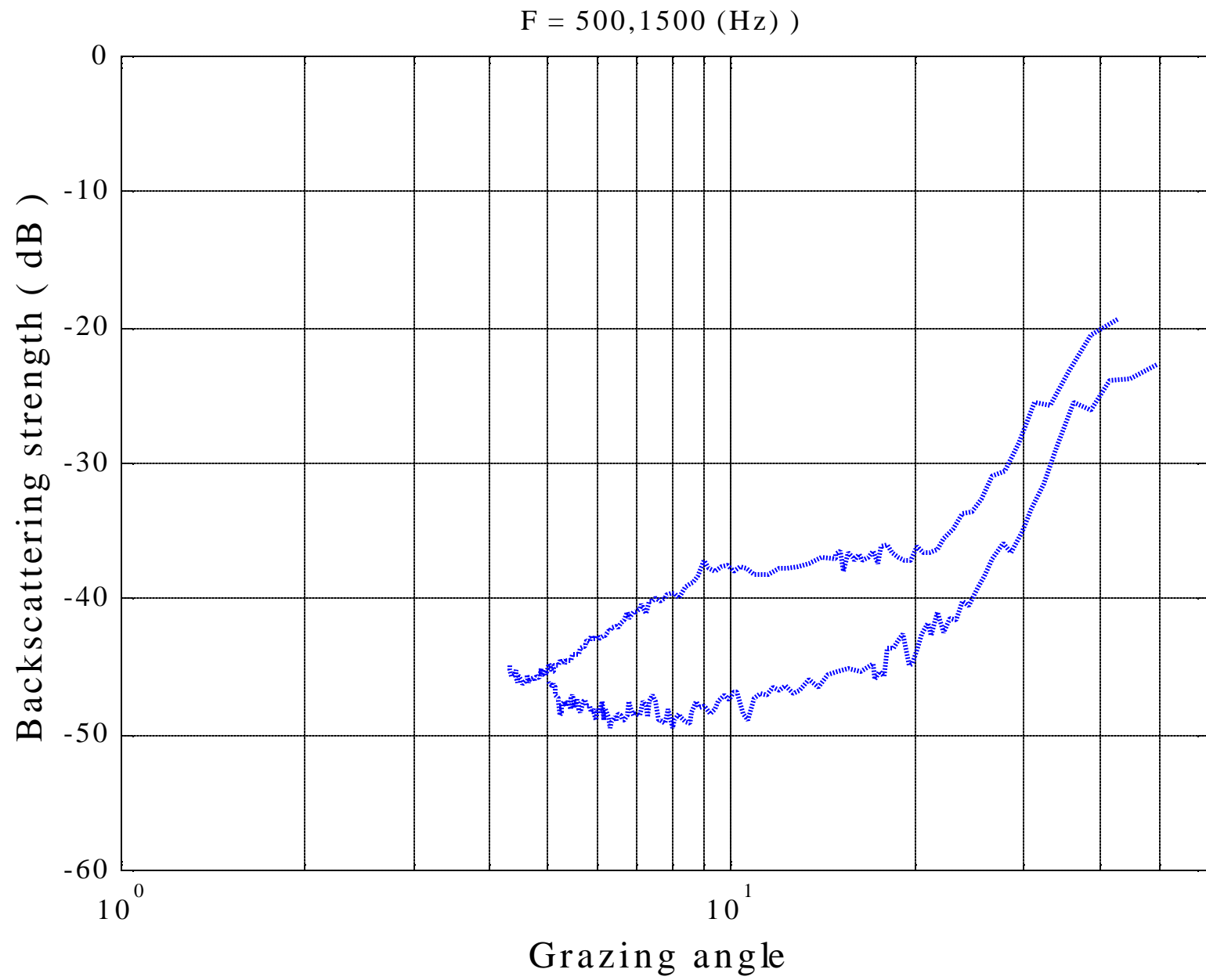


Inverted  $C_2$  from Rev.Coherence, East China Sea,06/03/01



seabed reflection coefficient -  $\ln |V(\theta)| = Q \theta$







## V. SUMMARY AND DISCUSSION

1. The RVC, expressed by the angular spectrum, has been converted back to a more familiar summation of normal-modes.
2. Measured RVC at 3 sites in the China Seas are in good agreement with the theoretical model.
3. The sound velocity and attenuation, inverted from RVC, are close to others, inverted from propagation data. Model/data comparisons show that the RVC can be a powerful characteristic for use in fast inversion of seabottom acoustic parameters (and in derivation of bottom scattering strength).
4. Be careful ! Different seabottom scattering models would cause some uncertainty on inversion results of bottom acoustic parameters. Thus, a scattering model with more physical base is desirable for numerical modeling. (under working )
5. For at-sea experiment design and lab data analyses on RVC, one needs carefully to consider the R/N noise ratio and  $\Delta z/\lambda$  ratio etc.

Thanks to  
IOA colleagues  
YS96 & ASIAEX team members  
for sharing data and helpful discussions